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TESTING THE CHARACTERISTICS OF FREE AND FORCED OSCILLATIONS ON FAP 2228 OFF-ROAD VEHICLE

Aleksandar Mićović* Technical Test Center, Belgrade, Serbia Dr Vladimir Popović Faculty of Mechanical Engineering, Belgrade, Serbia Dragoslava Mićović Academy of Criminalistic and Police Studies, Belgrade, Serbia Snežana Jovanović Technical Test Center, Belgrade, Serbia

The paper presents the testing of free and forced oscillations characteristics on FAP 2228 BS/A-45 off-road vehicle. The testing of free oscillations was conducted according to SORS 9127 (Standard of Defence of the Republic of Serbia) in laboratory conditions. The testing of forced oscillations was conducted in the course of driving on various surface paths - the heath in Deliblatska pescara, gravel at the territory of Fruska gora, on concrete surface at the runway of the Kovin airport, as well as on the asphalt surface of Belgrade-Šid highway. The testing was carried out according to SORS 0318 and ISO 2631 standards, and the results were evaluated according to 2002/44/EC Directive. Key words: FAP 2228 BS/A-45, Forced oscillations, Free oscillations, Testing, Comfort

INTRODUCTION

The concept of military vehicles refers primarily to engine-driven special purpose off-road vehicles. It covers various military systems driven by internal combustion engines, such as tanks, infantry armoured fighting vehicles, as well as a number of other special superstructures on offroad vehicles. This is exactly the group of vehicles which are not covered by ecological standards in practice.



Figure 1: FAP 2228 BS/A-45

As these vehicles are not used only during war, but also in peace time, it is necessary to establish the standards which must be applied in order to protect the health of their users. A special problem related to military vehicles results from the fact that they are very durable and last long, and therefore they do not fulfil the standards which the automobile industry started applying in the last ten years [05, 07]. Also, due to the special requirements set before the manufacturers regarding dynamic passability, the autonomous movement, the reliability of fitted components, as well as the accommodation of special equipment and weaponry, the price of manufacturing such vehicles is very high. It is a frequent case in practice that during the designing of superstructures to be installed on a basic type of a vehicle the constructors are faced with huge problems how to reduce the level of vibrations and noise inside the cabin to an acceptable level required for uninterrupted operation of the carrier [06, 08]. The main and transversal supports are connected by screws and rivets. The platform is equipped with JOST locks for container connecting. Overall dimensions of the vehicle are (length x width x height) 9,615 x 2,500 x 3,180 mm.

^{*} Technical Test Center, Vojvode Stepe 445, 11000 Belgrade, Serbia; amicovic1@gmail.com



FATIGUE AND VIBRATIONS

Military vehicles are primarily used in off-road, or all terrain conditions. When they are tested, the test drivers from Technical Testing Centre usually cover several thousands of kilometres on various surfaces and in various weather conditions, putting them to test by intensive driving.

Most of these vehicles are in prototype stage of development where various functional failures are possible. This is why the concentration of a test driver is of great importance for the safety of testing. However, the necessary consequence of intensive driving testing is the fatigue which occurs in operators [01]. According to a definition, fatigue is a phenomenon occurring as a consequence of the activities of a human body as a whole or an organic system in overcoming various types of burden defined by work requirements. Fatigue warns a body to cease the activity due to overburden and possible consequences. The important characteristic of fatigue is reversibility.

When they are in drive, all types of vehicles can be a sources of vibrations which are transfered to the whole body of a driver. The risk of health damage increases in people who are exposed to high level of vibrations on a regular basis and over the long term. In order to determine a daily exposure to vibrations (A(8)) or VDV (Vibration Dose Value), it is necessary to know the duration of total daily exposure to vibrations produced by vehicles used during the work process. Only the data referring to the concrete work process should be taken into account at that, i.e. only the time period during which a driver or a crew member was exposed to vibrations.

Testing of the human exposure to vibrations which are transferred to the whole body is carried out according to the method defined in ISSO 2631-1:1997, while the detailed instructions on the application of the vibration measuring method are given in the European Standard EN 14253:2003. The level of vibrations expressed as r. m. s. value (root-meansquare) is expressed as acceleration weighted considering frequency measured at the seat of a person sitting in the course of performing their work tasks, i.e. the feet of the person who is standing during the performance of their work tasks, and it is given as m/s². The level of vibrations expressed as r. m. s. value is equal to average acceleration measured in the interval of measurement conducted. This is the highest of the three values measured in three orthogonal axes (1.4 awx, 1.4 awy or awz) [09].

The alternative measure of the level of exposure to vibrations is Vibration Dose Value (VDV). VDV has been developed as a measure which represents a better risk indicator or exposure to vibrations with shocks. VDV is expressed in meter per second on 1.75th (m/s1.75) and as opposed to the level of vibrations expressed as r. m. s. value it represents a cumulative measuring result, i.e. it increases as the measuring time is prolonged. This is why it is important to know during all VDV measurements in which time period the value was measured. It should be the highest value measured in one of the three orthogonal axes (1,4 VDVwx, 1,4 VDVwy or VDVwz) [04].

Risk assessment must enable to recognize the method which can control the exposure to vibrations. When evaluating the exposure to vibrations, the work processes that cause them must also be taken into account. Understanding of the manner in which the workers are exposed to vibrations will help recognize the method for the reduction or complete elimination of this exposure [02, 03].

VIBRATION (FREE AND FORCED) MEASURING

Portable MAESTRO human vibration meter, manufactured by 01dB-Metravib, was used to measure the vibrations on the seats of both the driver and passengers in the vehicle cabin and the superstructure. This meter is intended primarily for human vibration measuring, i.e. measuring and calculating the influence on the human body (measurement of vibrations at the workplace which are transferred to the whole body or to the hands).

Alternatively, it is used to measure the level of noise (as four-channel system, the first three channels are intended for three-axis accelerometers, and the fourth channel can be connected to the oneaxis accelerometer or to a preamplifier with a microphone; it is adapted for measuring the efficiency of the seat and as a basic vibration meter).



Figure 2: Maestro





Figure 3: NetdB12

Its integration time ranges between 1 and 200 seconds and it has the possibility of start/stop mode, the memory capacity is 2 MB, as well as analogue output: 4-pin LEMO connector for signal recording or monitoring of all four channels within the range from 0.4 to 1000 Hz. The autonomous operation (when not plugged in mode) depends on the battery life and on an average it is from 8 to 13 hours. Free oscillations were measured by NetdB12 (01dB Metravib) vibro-acoustic measuring system manufactured by Areva, as well as NF piezoelectric accelerometers (type STS AS135/1A).

FREE OSCILLATIONS MEASURING

Testing of free oscillations was carried out in laboratory conditions on a flat concrete surface according to SORS 9127. The vehicle is equipped with dependent elastic suspension system on the front bridge with leaf springs, additional rubber cushions and telescopic hydraulic shock absorbers (left and right).

Measurements were carried out on two points:

- M_1 vehicle frame above the middle of the axle, and
- M₂ vehicle frame above the centre of the tandem of vehicle back axles.

Exciting a vehicle to natural oscillation is performed by stretching, i.e. free fall of the vehicle ends: front end for measuring point M₁ and rear end for M₂. Out of the recorded signal as evaluating parameters for free oscillations fo natural frequency and relative coefficient of damping Ψ are taken. As SORS 9127 refers to comfort characteristics – the evaluation of fo and Ψ parameters is given according to the criteria for human organism. From the recorded oscillation signals the values of fo and Ψ parameters were calculated in the form of damped sine wave and the results are shown in Table 1. On the front axle (M₁) the parameter of natural frequency suggests comfortable drive, while the coefficient of damping lies on the dividing line between comfortable and uncomfortable driving.

Vehicle	Measuring points	Parameters	Measured values	Comfort evaluation
FAP 2228 with container		f _o	2,3 Hz	Comfortable
	IVI ₁	Ψ	0,35	Conditionally comfortable
	M ₂	f _o	3 Hz	Conditionally comfortable
		Ψ	0,9	Uncomfortable

Table 1: Natural frequency f and relative coefficient of damping Ψ

On the measuring point at the centre of tandem axle (M_2) the parameter of natural frequency is within the range of conditionally comfortable driving, and the coefficient of damping suggests extremely uncomfortable driving. Table 2 shows the results of measuring the total weight of the vehicle with the container, as well as the weight distribution on the sides and axles.

In addition to the surface on which the vehicle is being driven, one of the most important parameters that have significant influence on measuring results is also the speed of the vehicle. This parameter has been chosen based on more than 20-year-long experience of the researchers of testing vehicles on testing paths in both Deliblatska pescara and Fruska gora. Realistic average speed on this type of surface is 30 km/h, but in order to obtain a more comprehensive insight into the measuring results and their comparison, the testing was also carried out at the speed of 40 km/h. Figures 4 through 6 show the examples of measuring results, while Table 3 shows the general results for all types of surfaces and all vehicle speeds.



				Vehicle without the container [kg]	Vehicle with the container [kg]		
Total weight, G _{tw}			,	10900	16100		
			Left wheel, G _{fl}	2400	2380		
Front axle			Right wheel, G _{fr}	2670	2620		
			Total, G _f	5070	5000		
NOI		Middle axle	Left wheel, G _{mi}	1550	2940		
IBUT			Right wheel, G _{mr}	1540	2920		
IGHT DISTRI			Total, G _m	3090	5860		
	Tandem axle	em axle Rear axle	Left wheel, G _{rl}	1360	2630		
			Right wheel, G _{rr}	1380	2610		
Ň			Total, G _r	2740	5240		
		Total tandem weight, $\mathbf{G}_{\mathbf{T}}$		5830	11100		
Left side of the vehicle, G				5310	7950		
Right side of the vehicle, G _r				5590	8150		

Table 2: Weight distribution on axles and sides

Table 3: General review of forced oscillations measuring results

Path	Measuring point	Speed (km/h)	Equivalent three- axle acceleration related to comfort $a_v (m/s^2)$	Comfort evaluation	Equivalent three- axle acceleration related to health a_v (m/s ²)	Recommended maximum exposure
	İ	50	0.78	somewhat	0.85	22h22m13s
	Driver	60	0.74	somewhat	0.81	23h54m28s
		70	0.73	somewhat	0.80	24h34m1s
		50	1.06	uncomfortable	1.13	11h7m22s
Asphalt	Codriver	60	1.04	uncomfortable	1.11	11h29m44s
		70	0.98	uncomfortable	1.04	12h55m2s
		40	0.64	somewhat	0.67	28h14m37s
	Crew	50	0.80	uncomfortable	0.84	18h17m1s
		60	1.33	very uncomfortable	1.40	6h43m18s
	Driver	60	0.88	uncomfortable	0.97	17h36m50s
Concrete		80	0.99	uncomfortable	1.08	13h28m10s
	Q a driver	50	1.11	uncomfortable	1.19	10h10m39s
	Codriver	70	1.05	uncomfortable	1.16	12h42m1s
	Driver	30	1.18	uncomfortable	1.36	11h38m31s
	Driver	40	1.64	very uncomfortable	1.87	5h38m41s
Heath	O a driven	30	1.36	very uncomfortable	1.50	7h26m32s
	Codriver	40	1.57	very uncomfortable	1.73	5h30m06s
	Ì	20	1.06	uncomfortable	1.12	10h22m39s
Gravel	Driver	Driver 30 1		very uncomfortable	1.63	6h42m55s
		40	1.17	uncomfortable	1.32	10h55m4s
		20	1.40	very uncomfortable	1.50	6h25m16s
	Codriver	30	1.37	very uncomfortable	1.48	6h50m31s
		40	1.64	very uncomfortable	1.77	4h43m41s
	Crow	30	0.99	uncomfortable	1.07	12h43m28s
	Ciew	40	1.43	very uncomfortable	1.51	5h46m11s



File	Vozac 4	40km l	MM1.c	mg					
Location									
Start	05-03-13 11:11:47								
End	05-03-13 11:13:25								
Whole body									
Quality	Health								
Body position	Seated								
Measurement location Seat									
	1	_	_				_		
Type	v	V	1	7	aw		Querell	Evenouuro	
Weighting	A NAG	T VA(d			Overall		A/0	Exposure	
Coefficient	1.4	1 4	VVd VVk		a		A(0)		
Level (m/s2)	0.65	0.63	1	37	1				
Corrected (m/s2)	0.91	0.89	1 1	37	1.8	7	1.37	8h	
Warning level (m/s2)	0.01	0.00			1.0		0.50	1h 4m 1s	
Maximum level (m/s2)							1.15	5h38m41s	
eVDV dose (m/s 1.75)	16.57	16.2	1 24	.97				8h	
Exposu	ire level a	A(8) is	above	e ma	ximur	n le	/el		
Туре				Ρ	eak fa	ctor	57.		
Axis	Х			Υ			Z	Max.	
Peak factor	3.4	8	1	8.15			3.68	3.68	
	Peak fa	ctor is	small	er th	an 9			й.	
According to Stand	lard 263	1-1, A((8) as:	sess	ment	is re	commer	nded	
Туре		-			VD\	/			
Axis	Х		Y	1	Z		Max.	Exposure	
Weighting	Wd	V	٧d	Wk		VDVeq			
Coefficient	1.4	1	.4		1				
VDV dose (m/s 1.75)	2.81	2	.67	6.	40				
Corrected (m/s 1.75)	3.94	3	.74	б.	40	0	6.40	1m38s	
Warning level (m/s 1.75)							3.10		
Maximum level (m/s 1.75)	in hole		min	n louo	4	1.00			
Y	DA IEAEI	is per	UW Wa	mm	g ieve				
File		V	ozac	: 40)km	M	11.cm	q	
Lasation								-	
Location		+							
Start		0	05-03-13 11:11:47						
End		0	05-03-13 11:13:25						
	W	hole	bo	dv					
Quality		C	Comfort						
Body position		s	Seated						
Magguromont los	10	Coot							
weasurementiou	10	eat							
Type						24	,		
1ype		V	_		av I	7 1	Outerall		
AXIS	-	X		Ŷ		2	Overall		
Weighting	Weighting				٧d		Wk	av	
Level (m/s2)	Level (m/s2)					1	.37	1.64	
1.25 m/s2 <= Ae	3 <= 2	.50	m/s	2:	very	ur	comfo	ortable	

Figure 4: Driver's seat, speed 40 km/h, heath

CONCLUSION

In order to obtain more comprehensive results on asphalt and concrete surfaces respectively, the measurements were carried out at constant speeds ranging from 40 to 80 km/h. Tests were made on the Kovin airport runway and on the part of highway near Sremska Mitrovica. Re-

File Vozac 80 Asfalt pista Kovin.cmg									
Location									
Start	art 14-11-1216:30:43								
End	14-11-1216:32:05								
Whole body									
Quality Health									
Body position	Seated								
Measurement location Seat									
Туре	aw								
Axis	X	Y	Z	Ove	Overall Overall		Exposure		
Weighting	Wd	Wd	Wk	a	/	A(8)			
Coefficient	1.4	1.4	1	_					
Level (m/s2)	0.34	0.28	0.89	3	-				
Corrected (m/s2)	0.48	0.39	0.8	9 1.0	98	0.89	8h		
Warning level (m/s2)						0.50	2h32m46s		
Maximum level (m/s2)		A (0) 1-			1	1.15	13h28m10s		
Exposur	e level	A(8) IS	abo	ve warn	ing	level			
Tune				Deel	. 60.0	1 a v			
Type	, N	1		Pear	Tac	7	Mov		
Axis Beak factor	2	10		1	+	202	101dX.		
Peak laciur	J.	10		0.10		3.83	3.03		
Peak factor is smaller than 9									
According to Standard 2631-1, A(8) assessment is recommended									
Tuno									
Axis	X		Y	7	Ť	Max	Exposure		
Weighting	NA/H	V	Vd	10/k	-	VDVeg	Exposure		
Coefficient	1.4	1	.4	1	-	10104			
VDV dose (m/s 1.75)	1.38	1	13	4.32	-				
Corrected (m/s 1.75)	1.94	1.	58	4.32		4.32	1m22s		
Warning level (m/s 1.75)					T	9.10			
Maximum level (m/s 1.75)	1					21.00			
VD	V level	is belo	w wa	arning le	evel				
	_		_						
File		Voza	ac 8	0 Ast	alt	pista K	ovin.cmg		
Location									
Start		14-11-1216:30:43							
Start		14-11-12 10.30.43							
End		14-11-1216:32:05							
	M	/hole	bo	dy					
Quality		Comfort							
Dedunceition		Control							
Body position		Sealed							
Measurement location Seat									
Туре				a	W				
Axis		Х		Y	Τ	Z	Overall		
Weighting		Wd		Wd		Wk	av		
Level (m/s2)	0.3	4	0.28		0.89	0.99			
0.80 m/s2 <= Aeq <= 1.60 m/s2 : uncomfortable									

Figure 5: Driver's seat, speed 80 km/h, asphalt

gardless of a relatively wide speed interval, the results obtained of the equivalent levels of vibrations at the driver's seat range from 0.9 to 1 m/s2 for the concrete surface and about 0.75 m/s2 for asphalt surface; it can, therefore, be concluded that various speeds on either concrete or asphalt surface do not have any significant influence on the level of vibrations on either driver's or co-driver's seat. It can be noticed that at the same speed the vibrations at the co-driver's seat are about 10% higher on a concrete surface, but also about 30% on the asphalt surface.



File	Suvozac 50 Asfalt pista Kovin.cmg								
Location									
Start	14-11-1216:34:06								
End	14-11-1216:35:47								
Whole body									
Quality	Health								
Body position	Seated								
Measurement location Seat									
Type		1.14		av	/				
Axis	X	Y	Z	Overa	II Overall	Exposure			
vveighting	vva	VVd	VVK	av	A(8)				
Coefficient	1.4	1.4	1	-					
Level (m/s2)	0.32	0.29	1.02	1.40	4.00	01			
Corrected (m/s2)	0.45	0.41	1.02	1.19	1.02	8n			
warning level (m/sz)					0.50	10b10m20S			
waximum iever (m/sz)	o lovel	A(9) in	abour	womin	0.000	1001000395			
Exposur	6 1646	A(0) IS	anove	s warnin	gievel				
Type Reak factor									
Axis	1	X	,	Y	7	Max.			
Peak factor	3	16	3	18	3.08	3.18			
Peak factor is smaller than 9									
According to Standard 2631-1, A(8) assessment is recommended									
			,						
Туре	ype VDV								
Axis	Х		Y	Z	Мах.	Exposure			
Weighting	Wd	٧	Vd	Wk	VDVeq				
Coefficient	1.4	1	.4	1					
VDV dose (m/s 1.75)	1.35	5 1.	24	4.19					
Corrected (m/s 1.75)	1.89	3 1.	73	4.19	4.19	1m41s			
Warning level (m/s 1.75)					9.10				
Maximum level (m/s 1.75)	L				21.00				
VD	v level	is belo	w war	ning leve	91				
File	1	Suvo	zar A	in Act	alt nieta	Kovin cma			
1 110		0010	Lac c	10 738	an piota	Rominering			
Location									
Start		14-11	1-12	16:34	:06				
End		14-11	1-12	16:35	47				
		Viholo	hod	v					
Quality	Ť	Comfort							
Quality	-+	Comion							
Body position		Seated							
Measurement locat	ion	n Seat							
Туре		aw							
Axis		Х		Y	Z	Overall			
Weighting	+	Wd		Wd	Wk	av			
Level (m(c2)	+	0.32	1	1.29	1.02	1.11			

0.80 m/s2 <= Aeq <= 1.60 m/s2 : uncomfortable Figure 6. Co-driver's seat, speed 50 km/h, asphalt

Considering that both seats (the driver's and codriver's) are equipped with the same type of seats, it can be concluded that the distribution of burder, as well as the choice of vehicle suspension system have influence on this irregularity. The oscillations measured during driving on the asphalt surface at the driver's and co-driver's seat suggest uncomfortable drive, particularly at the speed of 50 km/h.

Measuring of forced oscillations in the field following the comfort ability criteria suggests that driving at both the driver's and co-driver's seats can be classified as very uncomfortable on the macadam. This conclusion is also valid for the drive at the speed of 40 km/h on the heath. In general, the results for the co-driver's seat are more unfavorable. In regard to the criteria of harm to health, the driving in this off-road vehicle on both the heath and macadam surfaces should be limited in time until the stated warning levels of vibrations.

REFERENCES

- Bester, R.: The ride comfort versus handling decision for off-road vehicles, PhD thesis, Faculty of Engineering, Built environment and Information Technology (EBIT), University of Pretoria, Pretoria, 2006
- Blagojević I., Ivanović G., Janković S., Popović V. (2012): A model for gear shifting optimization in motor vehicles, Transactions of FAMENA, 36 2, pp.51-66
- Directive 2002/44/EC of the European Parliament and of the Council on the minimum health and safety requirements regarding the exposure of workers to the risks arising from physical agents (vibration), June 2002
- 4) ISO 2631 Mechanical vibration and shock
 Evaluation of human exposure to wholebody vibration, 1997
- Mikulić, D., Happ Z., Knezović M. (2004): Ecologically military vehicles, Hrvatski vojnik, No 109/110, pp 8-11
- Mićović, A., Popović, A., Jovanović, S. (2012): Acoustic testing inside cabin and passenger space of off-road vehicle land rover defender 110 soft top, Proceeding of Papers 23th National conference & 4th International conference - Noise and vibration, pp. 233 -235.
- Popović V., Vasić B., Rakićević B., Vorotović G. (2012): Optimization of maintenance concept choice using risk-decision factor – a case study, International Journal of Systems Science,4310, pp.1913-1926
- Stamenković D., Popović V., Spasojević-Brkić V., Radivojević J. (2011): Combination free replacement and pro-rata warranty policy optimization model, Journal of Applied Engineering Science, 9 ,pp. 457-464
- Smith S, (2008): Dynamic characteristics and human perception of vibration aboard a military propeller aircraft Air Force Research Laboratory, AFRL/RHPA, International Journal of Industrial Ergonomics 38, pp 868–879

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